

# Associated Engineering, LLC

103 S. Church Street - P.O. Box 1462 - Jonesboro, AR 72403 - Phone: (870) 932-3594 - Fax: (870) 935-1263

March 20, 2024

Mr. Michael Morris, PE City Engineering Department City of Jonesboro 300 South Church Street Jonesboro, AR 72401

Re:

Drainage Report – Farmer Hills Commercial Development

Southwest Drive Jonesboro, Arkansas

Dear Mr. Morris:

Attached is the Storm Water Analysis for the above referenced project. The site is located along Southwest Drive, across from the Southern Hills development. The site is currently a vacant commercial tract. The development is a C-3, Commercial Development.

Storm water runoff from on-site is collected and diverted to a drainage basin located along the west side of the project site and reduces the developed runoff to offset an increase of runoff to the east. By use of detention on the west side, peak storm water runoff is reduced from its previous condition to be 18% for the 10-year storm frequency event and 23% for the 100-year storm frequency event. Stormwater mitigation for each lot will be the responsibility of the future developer.

Should you have any questions or require additional information, please contact me.

Respectfully submitted,

John M. Easley, PE, PLS

Project Engineer

## Hydrograph Calculations

For

# Farmer Hills A Proposed Commercial Development Jonesboro, AR

Prepared by Associated Engineering, LLC John M. Easley, PE, PLS

March 19, 2024





# Drainage Report Farmer Hills A Proposed Commercial Development

Jonesboro, Arkansas March 19, 2024

#### Purpose:

The purpose of this report is to determine the storm drainage characteristics for a proposed commercial development located along Southwest Drive, across from the Southern Hills development. The site is currently a vacant wooded parcel.

#### Location:

The proposed development is located along Southwest Drive, across from the Southern Hills development. The site is currently a vacant commercial site.

#### Scope of Work:

Storm water runoff rates were computed using the United States Department of Interior's (USDI) Soil Conservation Service (SCS) 24-Hour Hydrograph Method. The method of calculation is computer generated using Hydroflow software. Maps of the site including off-site runoff onto the property were reviewed to provide data input for the computer program. Topographic information gathered from the field by Associated Engineering, LLC was used to determine these characteristics for the development.

The detention structure was reviewed for storage capabilities during the 2, 10, 25, 50 and 100-year storm frequency events. The detention configurations were also reviewed to determine any increase and/or decrease in the peak discharge of the associated storm events from the developed conditions. Storage routing of the developed hydrographs through the detention area were calculated by computer using Hydrograph software. The project site was reviewed for its runoff characteristics during the 2-year through 100-year storm frequency events for both existing and developed conditions.

#### **Overall Design:**

The project site is approximately 10 acres that is currently vacant and located on the west side of Southwest Drive. The development is currently wooded with a clear area for a overhead 69kv electric line (Entergy). The development will consist of three lots, two commercial lots adjacent to the proposed street and a third larger lot on the west end of the site. Future plans for the large lot have not been determined at this time. Drainage management and erosion control for the two commercial lots will be the responsibility of each lot. Stormwater mitigation for the proposed street will be constructed as part of initial development and a part of this design report. A detention basin will be placed on the west side of the site, near the end of the proposed street.

The general slope of the site is from the southeast corner to the northwest with site drainage leaving midway of the north line.

#### **Pre-Developed Flows:**

Calculations for the pre-developed flows for the 2-year through the 100-year storm frequency events are shown within Appendix "A". The basin is predominately Brandon-Saffell association - Hydrologic Soil Group "B". A summary of the input data and results are shown below:

#### Existing Basin:

```
Area = 7.2 acres
CN = 55 7.2 acres @ 55 = Woods
Tc = 13.6 minutes
```

#### **Post-Developed Flows:**

Calculations for the post-developed flows for the 2-year through the 100-year storm frequency events are shown within Appendix "A". A summary of the input data and results are shown below:

#### Developed Basin:

Computative analyses for the existing and developed conditions are shown within Appendix "A". A summary of the existing and combined developed data is shown below:

	Pre-	Post-	Percent	
Frequency	developed	developed	Change	
	Flows	Flows	in flows	
(year)	(cfs)	(cfs)	(cfs)	_
2-year	2.77	2.81	0%	
5-year	6.65	5.86	12%	
10-year	10.35	8.52	18%	
25-year	14.53	11.62	20%	
50-year	18.24	14.13	23%	
100-year	22.57	17.39	23%	
50-year	18.24	14.13	23%	

Detention Facility:

Basin Bottom: 377.00 Basin Top: 381.00

Outlet: 15° "V"Notch Weir

#### **Conclusions:**

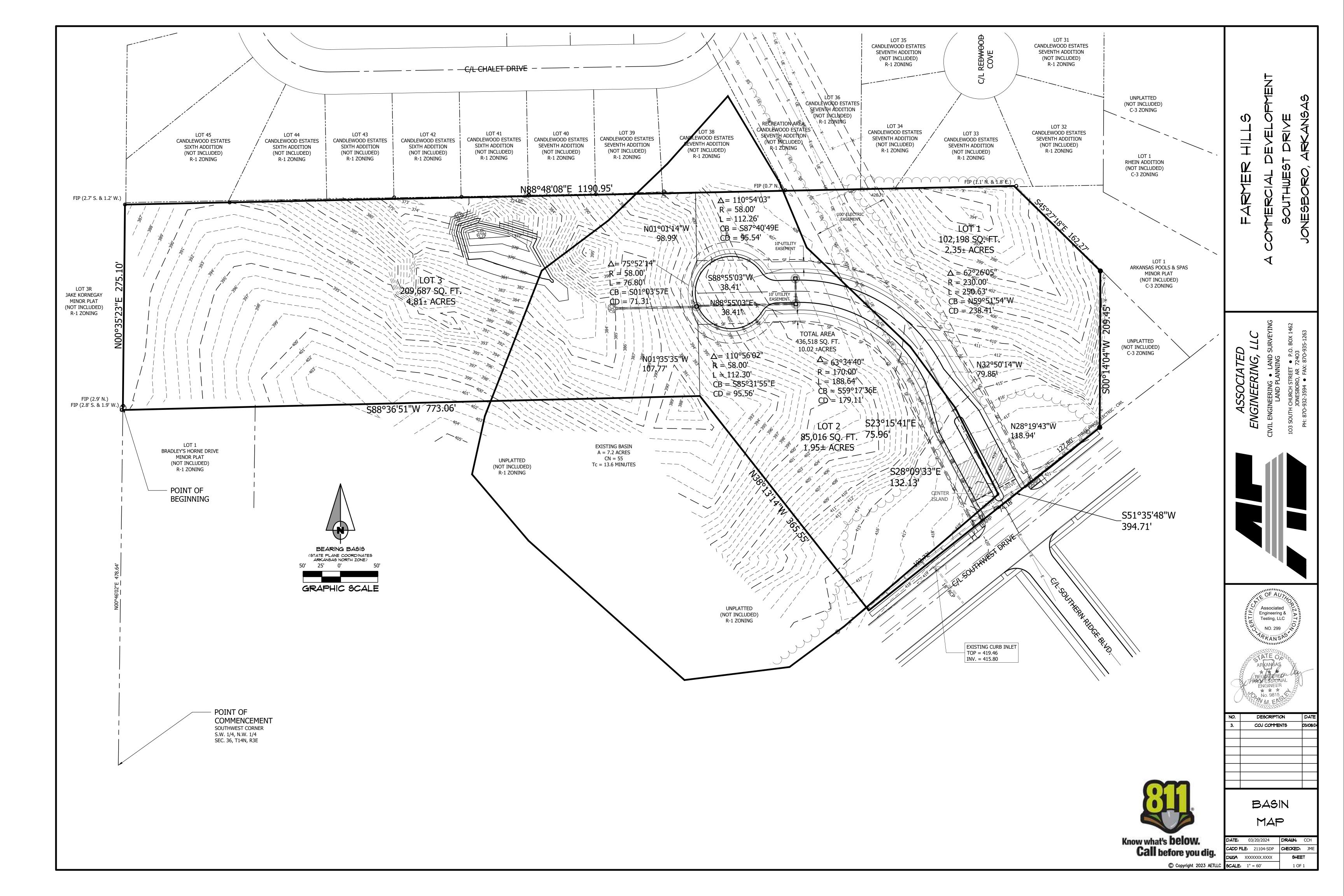
Based on and limited to the data and analysis and their applicability presented herein, the development, with the current structures, does not appear to endanger life or property, public or private.

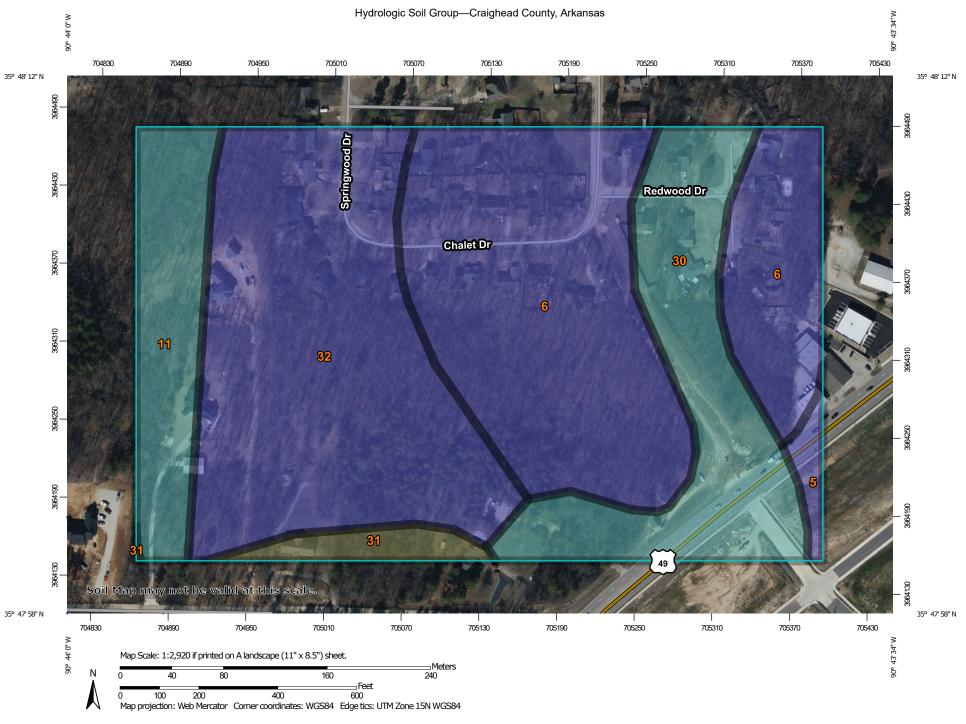
#### Appendix A

#### BASIN MAPS – EXISTING AND DEVELOPED

#### SOILS SURVEY PRINTOUT

HYDROGRAPH SUMMARY REPORT FOR PROPOSED COMMERCIAL DEVELOPMENT – FAMER HILLS: EXISTING AND DEVELOPED CONDITIONS FOR 2, 5, 10, 25, 50 AND 100-YEAR FREQUENCY EVENTS.





#### MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:20.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: Craighead County, Arkansas Survey Area Data: Version 23, Sep 8, 2023 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Feb 13, 2023—Feb 28. 2023 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

### **Hydrologic Soil Group**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
5	Brandon-Saffell association, moderately sloping	В	0.5	1.3%
6	Brandon-Saffell association, moderately steep	В	16.2	36.8%
11	Collins silt loam, 0 to 1 percent slopes, occasionally flooded, brief duration	С	4.2	9.6%
30	Loring silt loam, 3 to 8 percent slopes, west, upland phase	С	7.5	17.1%
31	Loring silt loam, 8 to 12 percent slopes, west	C/D	1.1	2.4%
32	Memphis silt loam, 12 to 40 percent slopes	В	14.4	32.9%
Totals for Area of Inter	est		43.9	100.0%

#### **Description**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

#### **Rating Options**

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

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2 -	Year	
	Summary Report	2
	Hydrograph Reports	
	Hydrograph No. 5, SCS Runoff, Existing Basin	
	TR-55 Tc Worksheet	
	Hydrograph No. 6, SCS Runoff, Existing Basini w Street	
	TR-55 Tc Worksheet	
	Hydrograph No. 7, Reservoir, <no description=""></no>	
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	Hydrograph Reports	
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	Hydrograph No. 7, Reservoir, <no description=""></no>	
10	- Year	
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	Hydrograph Reports	
	Hydrograph No. 5, SCS Runoff, Existing Basin	
	Hydrograph No. 6, SCS Runoff, Existing Basini w Street	
	Hydrograph No. 7, Reservoir, <no description=""></no>	
25	- Year	
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	Hydrograph Reports	
	Hydrograph No. 5, SCS Runoff, Existing Basin	
	Hydrograph No. 6, SCS Runoff, Existing Basini w Street	
	Hydrograph No. 7, Reservoir, <no description=""></no>	
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50	- Year	
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	Hydrograph No. 7, Reservoir, <no description=""></no>	

# Hydrograph Return Period Recap

	Hydrograph	Inflow				Peak Ou	tflow (cfs)	)			Hydrograph
No.	type (origin)	hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			1.545		2.983	4.261	5.672	6.906	8.327	Lot 1
2	SCS Runoff			0.736		0.919	1.063	1.211	1.333	1.469	SOTH HALF STREET
3	SCS Runoff			0.191		0.451	0.687	0.953	1.188	1.461	NORTH HALF 3
5	SCS Runoff			2.770		6.650	10.35	14.53	18.24	22.57	Existing Basin
6	SCS Runoff			4.132		8.603	12.63	17.12	21.07	25.67	Existing Basini w Street
7	Reservoir	6		2.807		5.856	8.521	11.62	14.13	17.39	<no description=""></no>

Proj. file: 21104.gpw

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# **Hydrograph Summary Report**

lyd. Hydrograph lo. type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1 SCS Runoff	1.545	2	720	4,173				Lot 1
2 SCS Runoff	0.736	2	716	1,737				SOTH HALF STREET
3 SCS Runoff	0.191	2	720	631				NORTH HALF 3
5 SCS Runoff	2.770	2	726	12,300				Existing Basin
6 SCS Runoff	4.132	2	724	15,578				Existing Basini w Street
7 Reservoir	2.807	2	732	15,563	6	378.34	1,709	<no description=""></no>

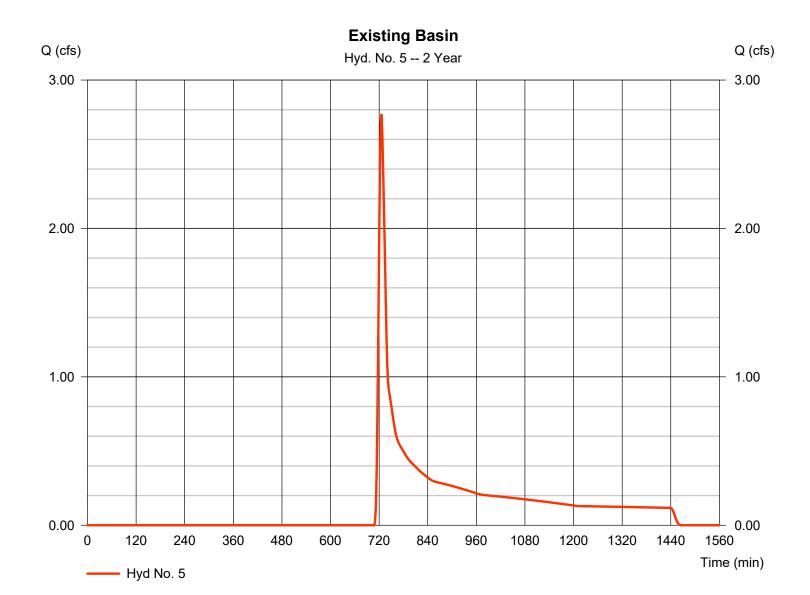
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#### Hyd. No. 5

**Existing Basin** 

= 2.770 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency = 2 yrsTime to peak = 726 min Time interval = 2 min Hyd. volume = 12,300 cuft= 7.200 acCurve number Drainage area = 55 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 13.60 min = TR55 Total precip. = 3.88 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



**Hyd. No. 5**Existing Basin

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 100.0 = 3.88 = 3.00		0.011 0.0 3.88 0.00		0.011 0.0 3.88 0.00		
Travel Time (min)	= 11.02	+	0.00	+	0.00	=	11.02
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 185.00 = 8.00 = Unpaved =4.56	d	415.00 5.00 Unpave 3.61	d	0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.68	+	1.92	+	0.00	=	2.59
Travel Time (min)  Channel Flow    X sectional flow area (sqft)    Wetted perimeter (ft)    Channel slope (%)    Manning's n-value    Velocity (ft/s)	= 0.68 = 0.00 = 0.00 = 0.015 =0.00	+	0.00 0.00 0.00 0.015 0.00	+	0.00 0.00 0.00 0.00 0.015	=	2.59
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value	= 0.00 = 0.00 = 0.00 = 0.015	+	0.00 0.00 0.00 0.015	+	0.00 0.00 0.00 0.015	=	2.59
Channel Flow  X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.00 = 0.015 =0.00	+	0.00 0.00 0.00 0.015 0.00	+	0.00 0.00 0.00 0.015	=	0.00

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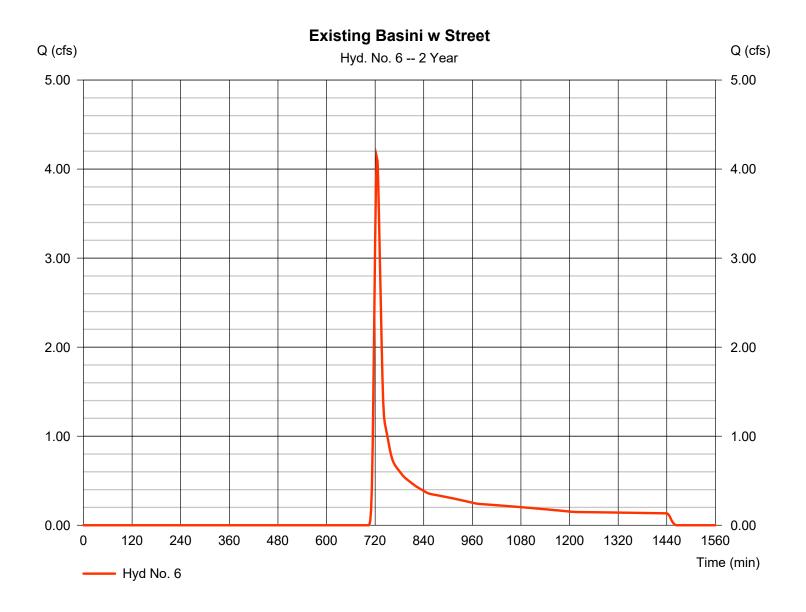
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#### Hyd. No. 6

Existing Basini w Street

Hydrograph type = SCS Runoff Peak discharge = 4.132 cfsStorm frequency = 2 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 15.578 cuft Drainage area = 7.200 acCurve number = 58\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method = TR55 Time of conc. (Tc)  $= 13.60 \, \text{min}$ Total precip. Distribution = Type II = 3.88 inShape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.500 \times 92) + (6.700 \times 55)] / 7.200$ 



**Hyd. No. 6**Existing Basini w Street

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 100.0 = 3.88 = 3.00	_	0.011 0.0 3.88 0.00		0.011 0.0 3.88 0.00	=	44.02
Travel Time (min)	- 11.02	+	0.00	+	0.00	_	11.02
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 185.00 = 8.00 = Unpaved =4.56	d	415.00 5.00 Unpave 3.61	d	0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.68	+	1.92	+	0.00	=	2.59
Channel Flow							
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.00 = 0.015 =0.00		0.00 0.00 0.00 0.015		0.00 0.00 0.00 0.015		
X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value	= 0.00 = 0.00 = 0.015 =0.00		0.00 0.00 0.015 0.00		0.00 0.00 0.015		
X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value	= 0.00 = 0.00 = 0.015		0.00 0.00 0.015		0.00 0.00 0.015		
X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.015 =0.00	+	0.00 0.00 0.015 0.00	+	0.00 0.00 0.015	=	0.00

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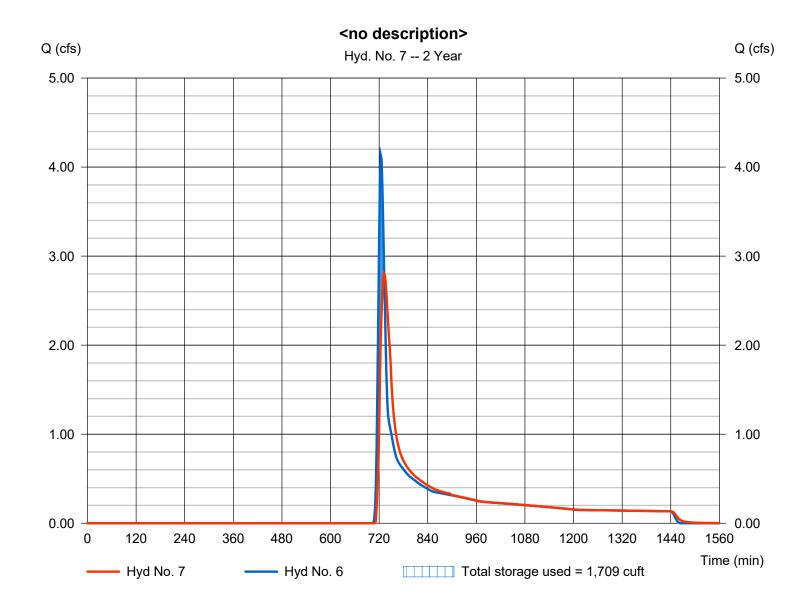
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#### Hyd. No. 7

<no description>

Hydrograph type = Reservoir Peak discharge = 2.807 cfsStorm frequency Time to peak = 732 min = 2 yrsTime interval = 2 min Hyd. volume = 15,563 cuftMax. Elevation Inflow hyd. No. = 6 - Existing Basini w Street = 378.34 ftReservoir name = POND 2 Max. Storage = 1,709 cuft

Storage Indication method used.



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#### Pond No. 3 - POND 2

#### **Pond Data**

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 376.00 ft

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	376.00	10	0	0
1.00	377.00	387	153	153
2.00	378.00	1,380	833	986
3.00	379.00	2,944	2,113	3,099
4.00	380.00	5,006	3,929	7,028
5.00	381.00	7,608	6,261	13,289

#### **Culvert / Orifice Structures Weir Structures** [A] [B] [C] [PrfRsr] [A] [B] [C] [D] = 0.00 0.00 0.00 = 0.00 0.00 0.00 Rise (in) 0.00 Crest Len (ft) 0.00 Span (in) = 0.000.00 0.00 0.00 Crest El. (ft) = 376.00 0.00 0.00 0.00 No. Barrels = 00 Weir Coeff. = 0.333.33 3.33 3.33 Invert El. (ft) = 0.000.00 0.00 0.00 Weir Type = 15 degV Length (ft) = 0.000.00 0.00 0.00 Multi-Stage No No No = No Slope (%) = 0.000.00 0.00 n/a n/a N-Value = .013 .013 .013 = 0.60 0.60 0.60 0.60 Exfil.(in/hr) = 0.000 (by Wet area) Orifice Coeff. Multi-Stage = n/a No No No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

#### Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	CIv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	376.00											0.000
1.00	153	377.00					0.33						0.334
2.00	986	378.00					1.89						1.889
3.00	3,099	379.00					5.21						5.207
4.00	7,028	380.00					10.69						10.69
5.00	13,289	381.00					18.67						18.67

# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	2.983	2	720	7,236				Lot 1
2	SCS Runoff	0.919	2	716	2,188				SOTH HALF STREET
3	SCS Runoff	0.451	2	720	1,172				NORTH HALF 3
5	SCS Runoff	6.650	2	724	22,847				Existing Basin
6	SCS Runoff	8.603	2	724	27,432				Existing Basini w Street
	Reservoir	5.856	2	732	27,417	6	379.14	3,664	<no description=""></no>
211	04.gpw	1	1	1	Return f	Period: 5 Ye	ear	Tuesday, (	03 / 19 / 2024

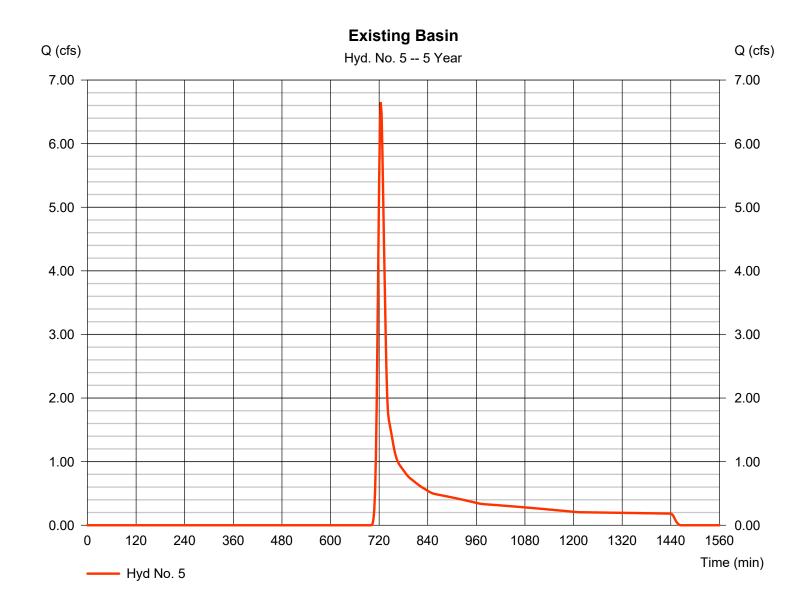
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#### Hyd. No. 5

#### **Existing Basin**

Hydrograph type = SCS Runoff Peak discharge = 6.650 cfsStorm frequency = 5 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 22,847 cuft Drainage area = 7.200 acCurve number = 55 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 13.60 min = TR55 Total precip. = 4.83 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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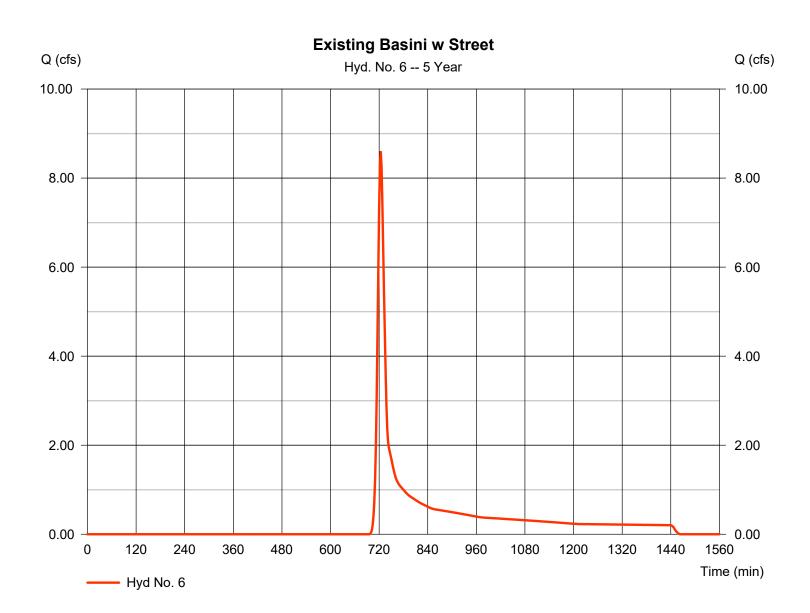
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#### Hyd. No. 6

Existing Basini w Street

Hydrograph type = SCS Runoff Peak discharge = 8.603 cfsStorm frequency Time to peak = 724 min = 5 yrsTime interval = 2 min Hyd. volume = 27.432 cuft = 7.200 acCurve number Drainage area = 58\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = TR55  $= 13.60 \, \text{min}$ Total precip. = 4.83 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.500 \times 92) + (6.700 \times 55)] / 7.200$ 



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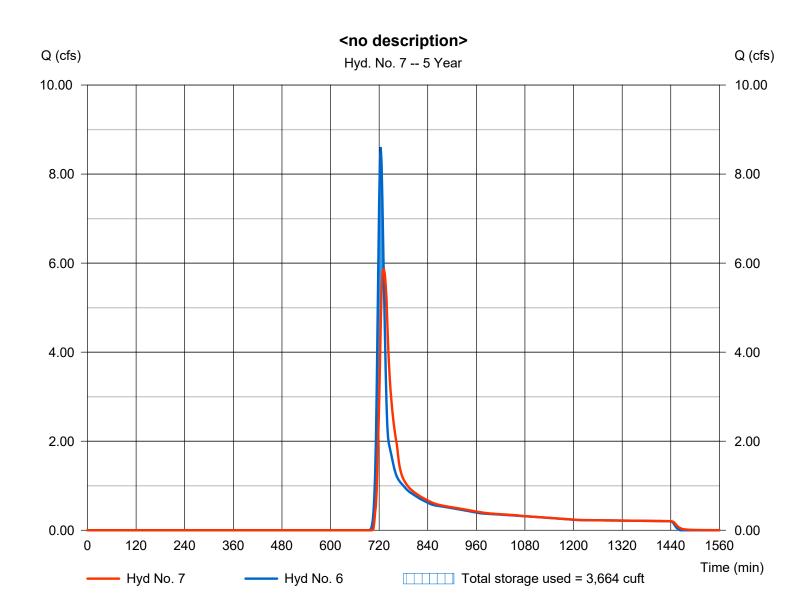
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#### Hyd. No. 7

<no description>

Hydrograph type = Reservoir Peak discharge = 5.856 cfsStorm frequency = 5 yrsTime to peak = 732 min Time interval = 2 min Hyd. volume = 27,417 cuftMax. Elevation Inflow hyd. No. = 6 - Existing Basini w Street = 379.14 ftReservoir name = POND 2 Max. Storage = 3,664 cuft

Storage Indication method used.



# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	4.261	2	720	10,013				Lot 1
2	SCS Runoff	1.063	2	716	2,545				SOTH HALF STREET
3	SCS Runoff	0.687	2	720	1,676				NORTH HALF 3
5	SCS Runoff	10.35	2	724	32,683				Existing Basin
6	SCS Runoff	12.63	2	724	38,249				Existing Basini w Street
:11	04.gpw				Return I	Period: 10 `	Year	Tuesday, (	03 / 19 / 2024

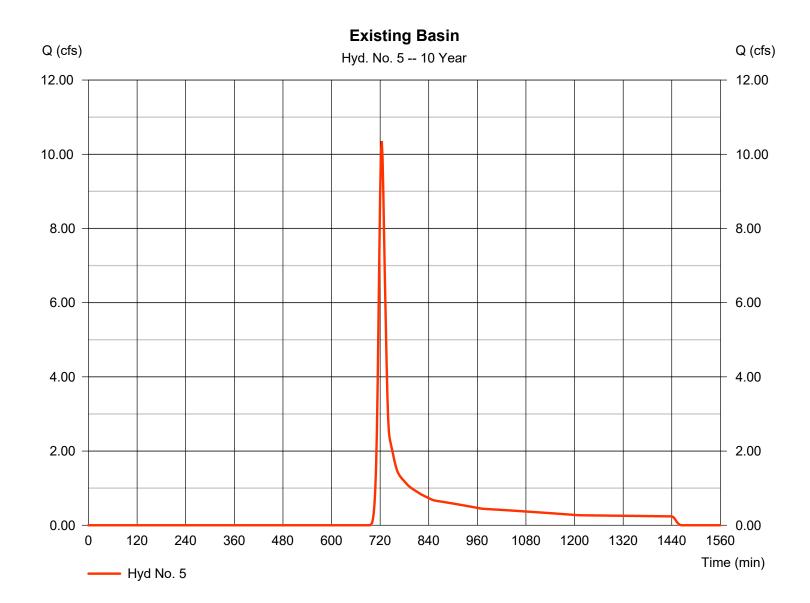
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

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#### Hyd. No. 5

**Existing Basin** 

Hydrograph type = SCS Runoff Peak discharge = 10.35 cfsStorm frequency = 10 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 32,683 cuft = 7.200 acCurve number Drainage area = 55 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 13.60 min = TR55 Total precip. = 5.58 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2020

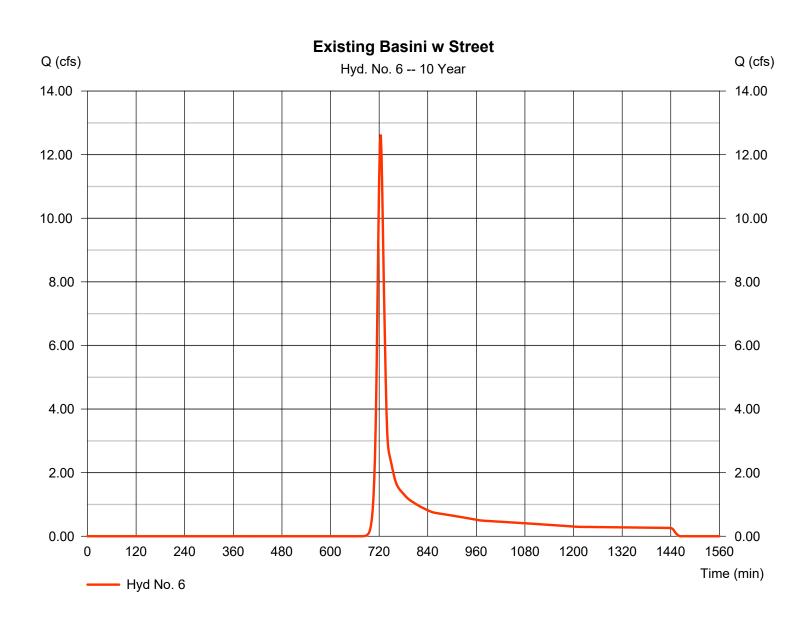
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#### Hyd. No. 6

Existing Basini w Street

Hydrograph type = SCS Runoff Peak discharge = 12.63 cfsStorm frequency = 10 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 38.249 cuft = 7.200 acCurve number Drainage area = 58\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = TR55  $= 13.60 \, \text{min}$ Total precip. = 5.58 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.500 \times 92) + (6.700 \times 55)] / 7.200$ 



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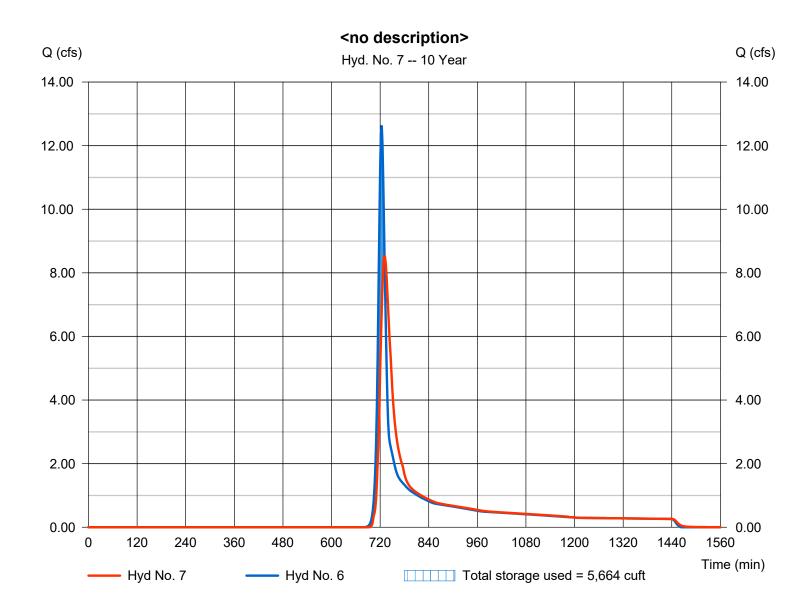
Tuesday, 03 / 19 / 2024

#### Hyd. No. 7

<no description>

Hydrograph type = Reservoir Peak discharge = 8.521 cfsStorm frequency = 10 yrsTime to peak = 730 min Time interval = 2 min Hyd. volume = 38,235 cuft Max. Elevation Inflow hyd. No. = 6 - Existing Basini w Street = 379.65 ftReservoir name = POND 2 Max. Storage = 5,664 cuft

Storage Indication method used.



# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	5.672	2	720	13,124				Lot 1
2	SCS Runoff	1.211	2	716	2,912				SOTH HALF STREET
3	SCS Runoff	0.953	2	720	2,252				NORTH HALF 3
5	SCS Runoff	14.53	2	724	43,906				Existing Basin
6	SCS Runoff	17.12	2	724	50,421				Existing Basini w Street
211	04.gpw	1	1	1	Return I	□ Period: 25 `	∸ Year	Tuesday, 0	03 / 19 / 2024

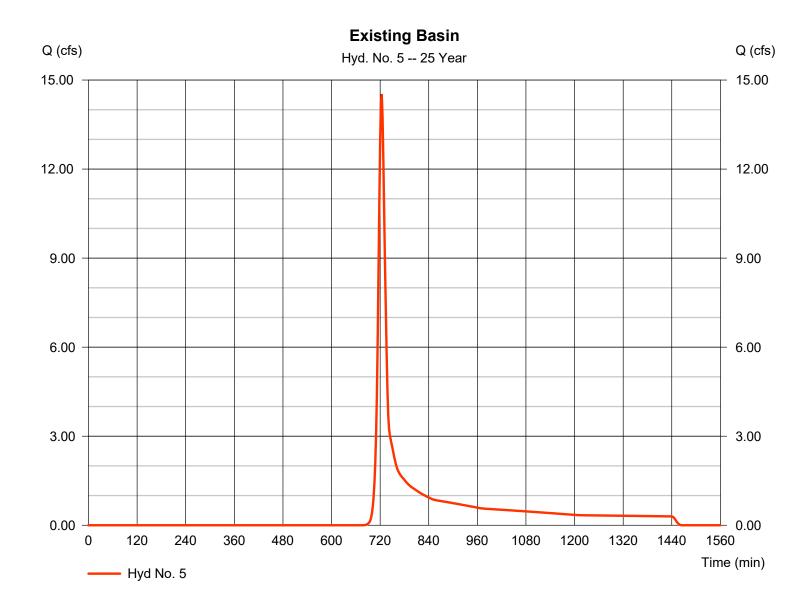
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#### Hyd. No. 5

#### **Existing Basin**

Hydrograph type = SCS Runoff Peak discharge = 14.53 cfsStorm frequency = 25 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 43,906 cuft = 7.200 acCurve number Drainage area = 55 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 13.60 min = TR55 Total precip. = 6.35 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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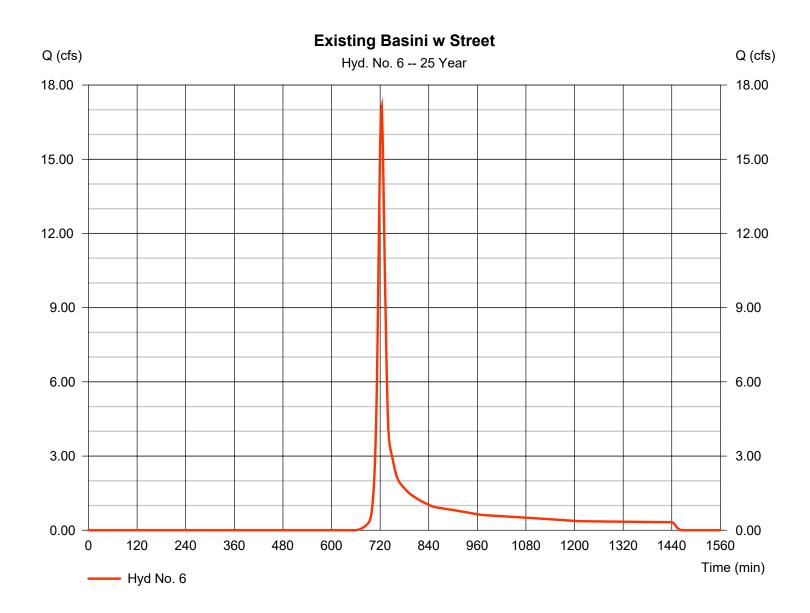
Tuesday, 03 / 19 / 2024

#### Hyd. No. 6

Existing Basini w Street

Hydrograph type = SCS Runoff Peak discharge = 17.12 cfsStorm frequency = 25 yrs Time to peak = 724 min Time interval = 2 min Hyd. volume = 50.421 cuft = 7.200 acCurve number Drainage area = 58\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = TR55  $= 13.60 \, \text{min}$ Total precip. = 6.35 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.500 \times 92) + (6.700 \times 55)] / 7.200$ 



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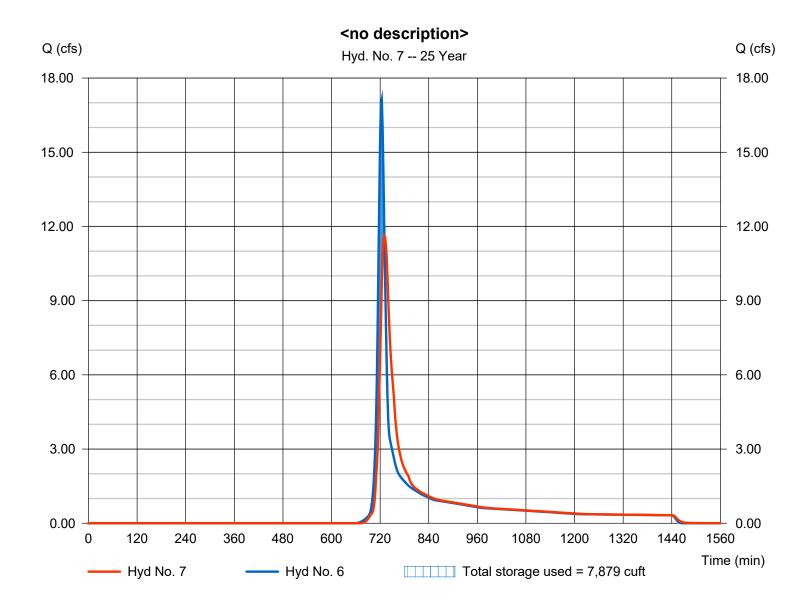
Tuesday, 03 / 19 / 2024

#### Hyd. No. 7

<no description>

Hydrograph type = Reservoir Peak discharge = 11.62 cfsStorm frequency = 25 yrsTime to peak = 730 min Time interval = 2 min Hyd. volume = 50,407 cuftMax. Elevation Inflow hyd. No. = 6 - Existing Basini w Street = 380.14 ftReservoir name = POND 2 Max. Storage = 7,879 cuft

Storage Indication method used.



# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description	
1	SCS Runoff	6.906	2	720	15,875				Lot 1	
2	SCS Runoff	1.333	2	716	3,216				SOTH HALF STREET	
3	SCS Runoff	1.188	2	720	2,767				NORTH HALF 3	
5	SCS Runoff	18.24	2	724	53,959				Existing Basin	
6	SCS Runoff	21.07	2	724	61,221				Existing Basini w Street	
7	Reservoir	14.13	2	730	61,206	6	380.47	9,987	<no description=""></no>	
21104.gpw					Return I	Return Period: 50 Year			Tuesday, 03 / 19 / 2024	

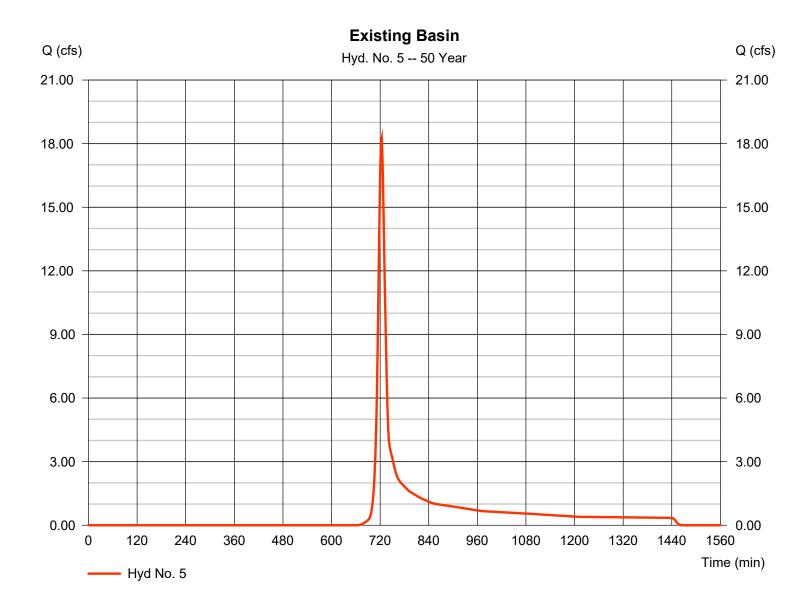
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#### Hyd. No. 5

**Existing Basin** 

Hydrograph type = SCS Runoff Peak discharge = 18.24 cfsStorm frequency = 50 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 53,959 cuftDrainage area = 7.200 acCurve number = 55 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 13.60 min = TR55 Total precip. = 6.99 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



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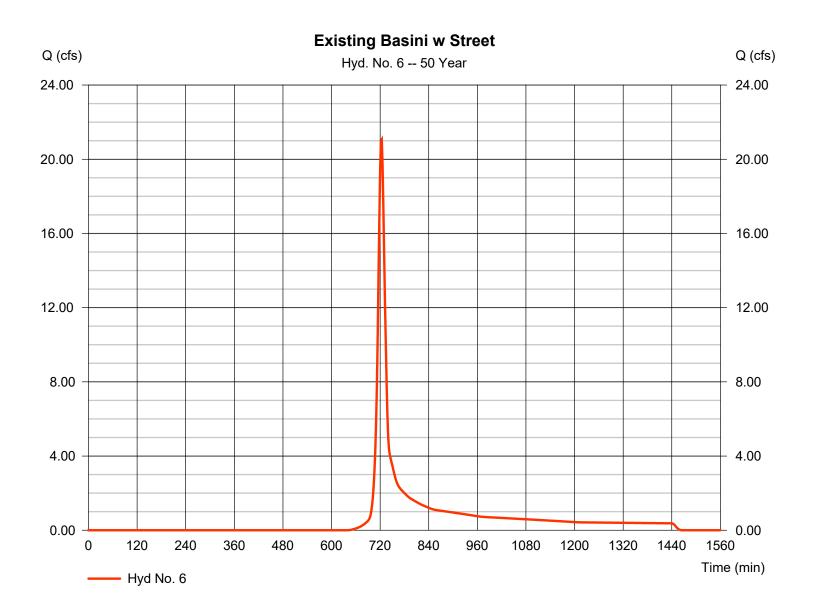
Tuesday, 03 / 19 / 2024

#### Hyd. No. 6

Existing Basini w Street

Hydrograph type = SCS Runoff Peak discharge = 21.07 cfsStorm frequency = 50 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 61.221 cuft = 7.200 acCurve number Drainage area = 58\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = TR55  $= 13.60 \, \text{min}$ Total precip. = 6.99 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.500 \times 92) + (6.700 \times 55)] / 7.200$ 



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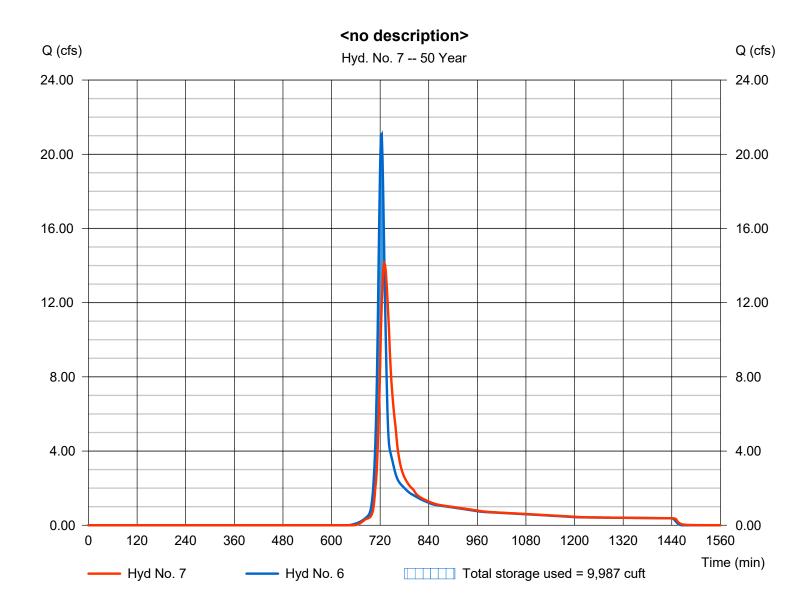
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#### Hyd. No. 7

<no description>

Hydrograph type = Reservoir Peak discharge = 14.13 cfsStorm frequency = 50 yrsTime to peak = 730 min Time interval = 2 min Hyd. volume = 61,206 cuft = 6 - Existing Basini w Street Max. Elevation Inflow hyd. No. = 380.47 ftReservoir name = POND 2 Max. Storage = 9,987 cuft

Storage Indication method used.



# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	8.327	2	720	19,077				Lot 1
2	SCS Runoff	1.469	2	716	3,554				SOTH HALF STREET
3	SCS Runoff	1.461	2	720	3,373				NORTH HALF 3
5	SCS Runoff	22.57	2	724	65,771				Existing Basin
6	SCS Runoff	25.67	2	722	73,813				Existing Basini w Street
	Reservoir		2	730	73,798	6	380.86	12,409	<no description=""></no>
	04.gpw				Return I			Tuesday, (	

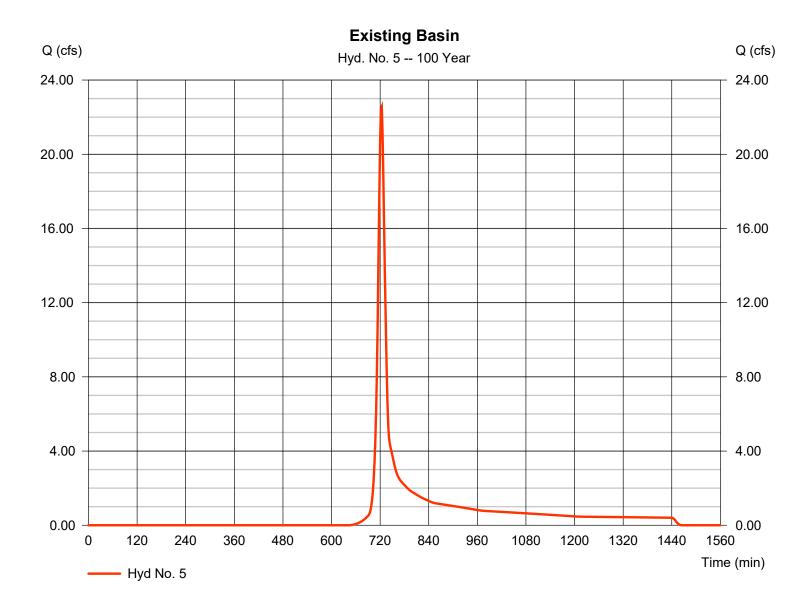
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#### Hyd. No. 5

**Existing Basin** 

= 22.57 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency = 100 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 65,771 cuft= 7.200 acCurve number Drainage area = 55 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 13.60 min = TR55 Total precip. = 7.70 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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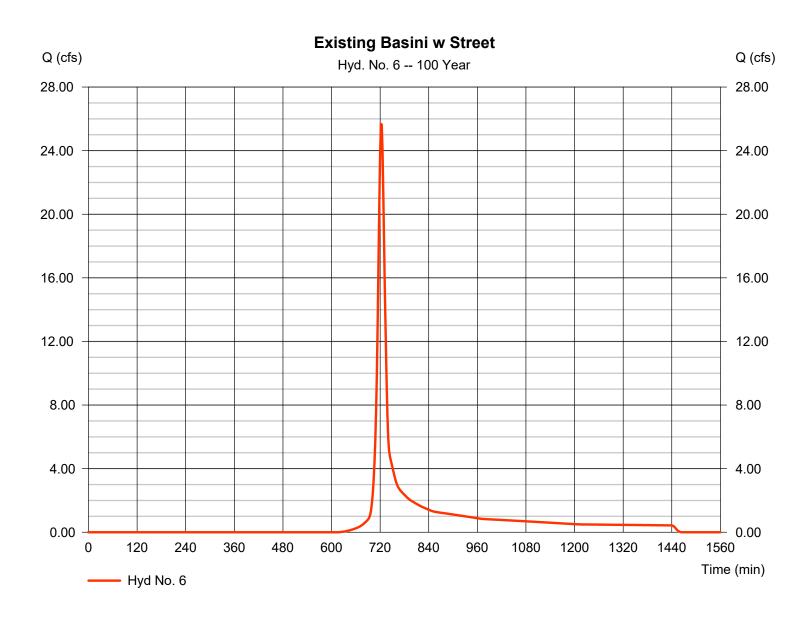
Tuesday, 03 / 19 / 2024

#### Hyd. No. 6

Existing Basini w Street

Hydrograph type = SCS Runoff Peak discharge = 25.67 cfsStorm frequency = 100 yrsTime to peak = 722 min Time interval = 2 min Hyd. volume = 73.813 cuft = 7.200 acCurve number Drainage area = 58\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = TR55  $= 13.60 \, \text{min}$ Total precip. Distribution = Type II = 7.70 inShape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.500 \times 92) + (6.700 \times 55)] / 7.200$ 



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#### Hyd. No. 7

<no description>

Hydrograph type = Reservoir Peak discharge = 17.39 cfsStorm frequency Time to peak = 730 min = 100 yrsTime interval = 2 min Hyd. volume = 73,798 cuft = 6 - Existing Basini w Street Max. Elevation Inflow hyd. No. = 380.86 ftReservoir name = POND 2 Max. Storage = 12,409 cuft

Storage Indication method used.

